

PROBABILISTIC ASSESSMENT OF RAILWAY TURNOUTS USING A MULTIBODY SIMULATION SOFTWARE

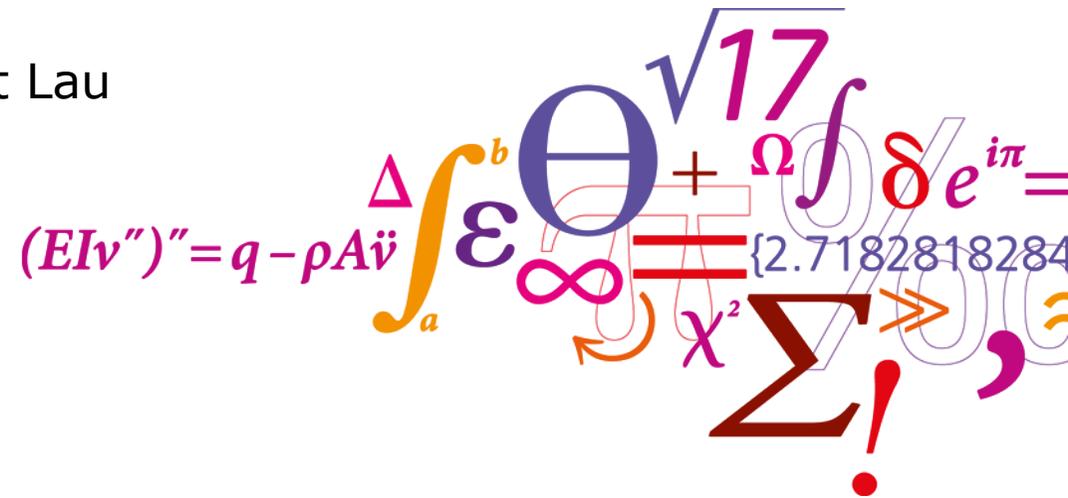
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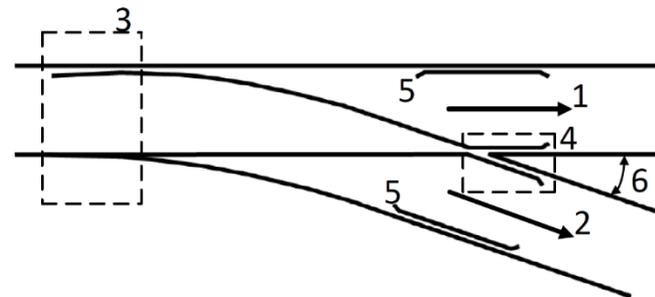


Outline of presentation

- 1) Motivation
- 2) Objective
- 3) General railway dynamics
- 4) Numerical modelling of railway turnout
- 5) Probabilistic method
- 6) Probabilistic assessment of turnout model
- 7) Concluding and reflecting remarks

Motivation

- Switches & crossings (S&Cs) exposed to accelerated degradation process
- Failure leads to **derailment** of trains
- Around 50 % of condition-based maintenance required for 3500 switches & crossings in Danish railway network
- Unscheduled repair of S&Cs are responsible for a significant portion of temporary speed reductions and associated delays



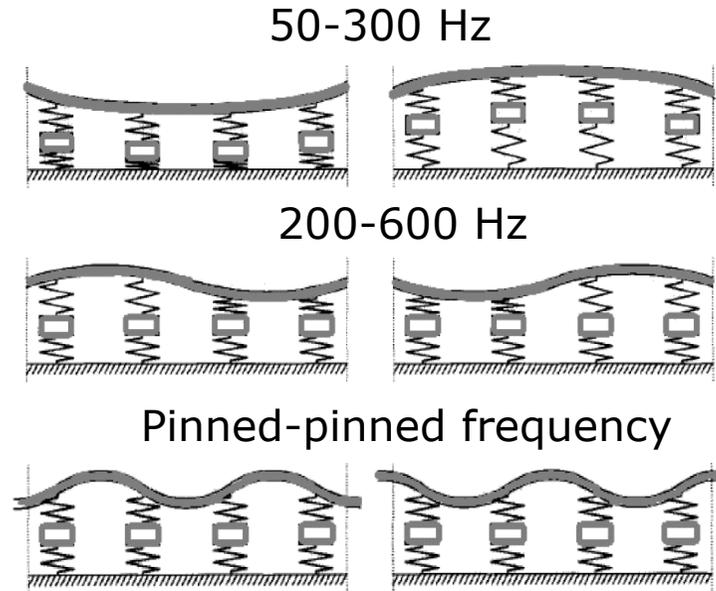
Objective

- Perform a probabilistic assessment of the accelerations of the train as these are related to degradation when the train travels through a turnout in the diverging track
- Probabilistic assessment provides information about:
 - 1) Level and uncertainty of accelerations
 - 2) Importance of train and track components

General dynamic properties

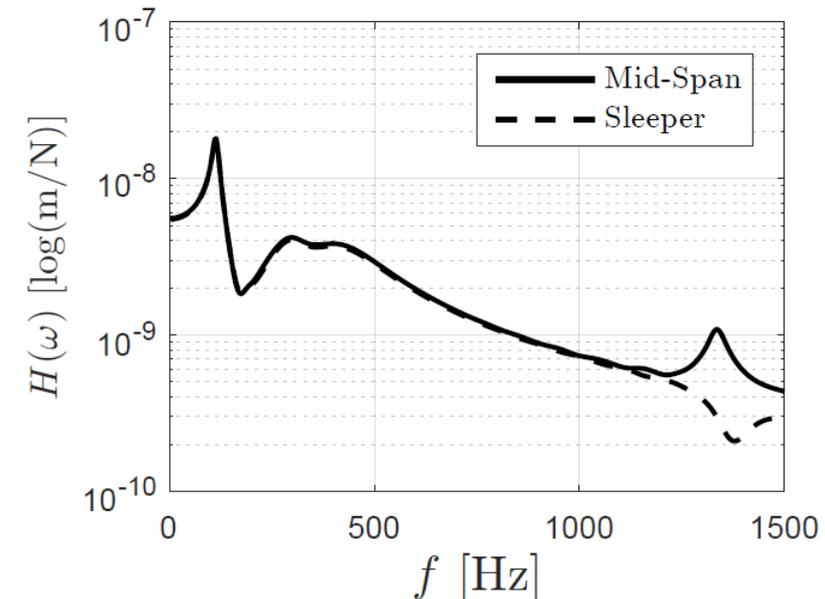
- Sleeper-passing frequency and effect
- Coupled train-track resonance 30-100 Hz
- Three track related resonant frequencies

Track mode shapes related to three main resonance frequencies:



Courtesy of Alejandro de Miguel (2015)

Typical receptance curve:



Numerical modelling

- Multibody simulation software: GENSYS

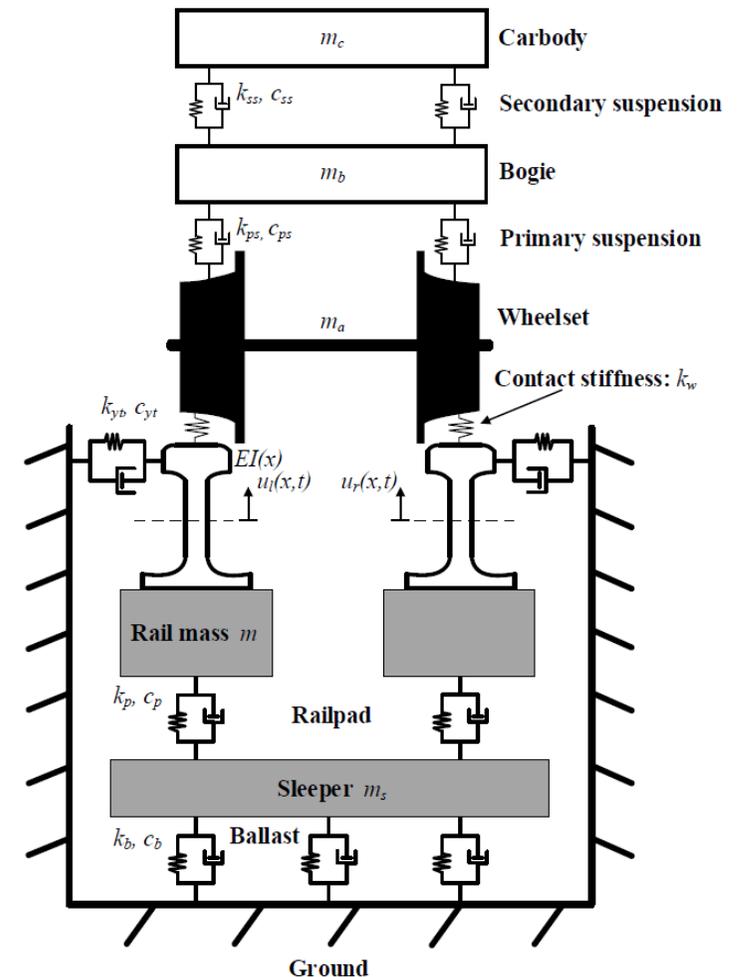
Characteristics:

- Rigid bodies connected by massless flexible elements
- Detailed rail and wheel profiles -> Accurate contact analysis
- Low computational time compared to FEM

- Euler-Bernoulli Track (EBT) model

- A fixed track taking into account the rail bending effect.
- Realistic model capturing general railway dynamic characteristics.

Credit: A. de Miguel, I. Santos, I. Hoff & A. Lau



Methodology of probabilistic assessment

- Based on uncertainty and sensitivity analysis that assume the input variables to be stochastic and independent
- Uncertainty analysis includes:
 - Monte Carlo simulation
- Sensitivity analysis includes:
 - Elementary effects method (EEM)

Monte Carlo simulation

- Sample matrix holding N samples for k input variables:

$$\begin{bmatrix} X_1^{(1)} & X_2^{(1)} & X_3^{(1)} & \dots & X_k^{(1)} \\ X_1^{(2)} & X_2^{(2)} & X_3^{(2)} & \dots & X_k^{(2)} \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ X_1^{(N-1)} & X_2^{(N-1)} & X_3^{(N-1)} & \dots & X_k^{(N-1)} \\ X_1^{(N)} & X_2^{(N)} & X_3^{(N)} & \dots & X_k^{(N)} \end{bmatrix}$$

- Compute model output for each sample to obtain:

$$\mathbf{Y} = \begin{pmatrix} Y^{(1)} \\ Y^{(2)} \\ \vdots \\ Y^{(N-1)} \\ Y^{(N)} \end{pmatrix}$$

- The uncertainty is quantified through mean and variance of \mathbf{Y}
- The uncertainty is visualized by plotting the output distribution in a bar plot

Elementary Effects Method

- Use multiple samples of wide ranges of variations to remove dependency of single sample point
- Idea of EEM owed to Morris who defined the elementary effect of i th input as:

$$EE_i = \frac{Y(X_1, X_2, \dots, X_{i-1}, X_i + \Delta, \dots, X_k) - Y(X_1, X_2, \dots, X_k)}{\Delta}$$

- Effectiveness of EEM relies on sampling strategy. Using p -levels of input factors, a trajectory is build from:

$$\mathbf{B}^* = \left(\mathbf{J}_{k+1,1} \mathbf{x}^* + \frac{\Delta}{2} ((2\mathbf{B} - \mathbf{J}_{k+1,k}) \mathbf{D}^* + \mathbf{J}_{k+1,k}) \right) \mathbf{P}^*$$

- Best combination of r trajectories determined from largest Euclidean distances between them
- Importance of input variables determined through evaluation of three statistics:

$$\mu_i^* = \frac{1}{r} \sum_{j=1}^r |EE_i^j| \quad \mu_i = \frac{1}{r} \sum_{j=1}^r EE_i^j \quad \sigma_i^2 = \frac{1}{r-1} \sum_{j=1}^r (EE_i^j - \mu_i)^2$$

Probabilistic assessment of turnout model

- EBT Turnout model with specifications:

S&C:

Type: 60E1-760-1:15r

Length: 120 m

30 rail cross sections

400 rail masses

200 sleeper masses

Train:

Passenger flirt train with single car body

Bogie base distance: 16.8 m

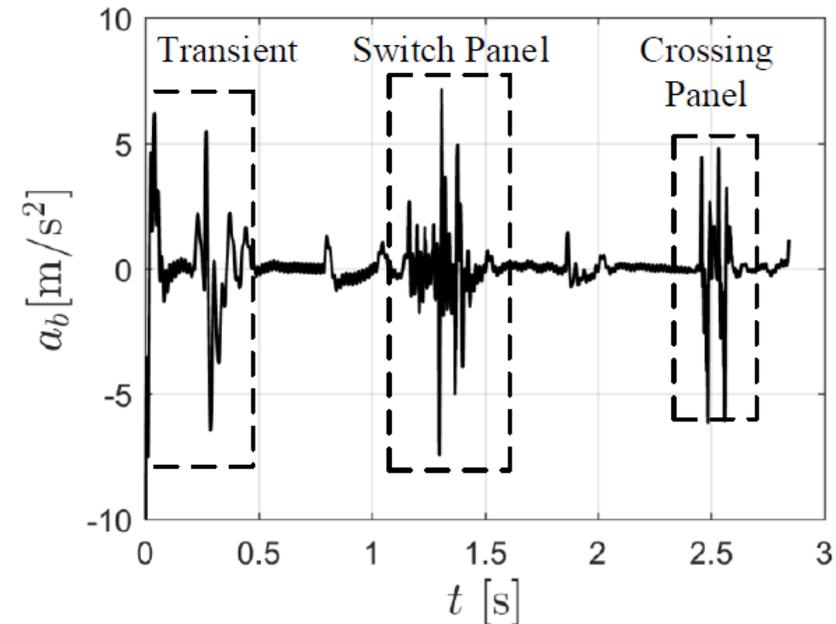
Wheelset base distance: 2.5 m

Wheel profile: S1002

- Reference measure

- Accelerations of train related to degradation by Lopez Pita(2006)
- Convenient because these can be measured practically

Vertical accelerations of train:



Used to establish two model outputs: Y_s and Y_c

Probabilistic assessment of turnout model

- Stochastic variables:

Parameter	min/mean	max/std	Distribution	Source
Ballast stiffness k_b	165 MN/m	220 MN/m	Uniform	[9]
Ballast damping c_b	55 kNs/m	82 kNs/m	Uniform	[9]
Sleeper mass m_s	129 kg/m	1.29 kg/m	Normal	[7]
Railpad stiffness k_p	53 MN/m	600 MN/m	Uniform	[15] + [9]
Railpad damping c_p	30 kNs/m	63 kNs/m	Uniform	[9]
Rail mass m	60 kg/m	0.60 kg/m	Normal	[7]
Bending stiffness EI	$6.043 \times 10^6 \text{ Nm}^2$	$3.0215 \times 10^4 \text{ Nm}^2$	Normal	[7]

Parameter	min/mean	max/std	Distribution	Source
Bogie mass m_b	2.32 t	3.48 t	Uniform	[15]
Wheelset mass m_a	1.6 t	2 t	Uniform	[15]
Speed v	120 km/h	2 km/h	Normal	[2]
Prim. susp. stiffness k_{ps}	1300 kN/m	3900 kN/m	Uniform	[15]
Prim. susp. damping c_{ps}	6 kNs/m	18 kNs/m	Uniform	[15]
Sec. susp. stiffness k_{ss}	290 kN/m	870 kN/m	Uniform	[15]
Sec. susp. damping c_{ss}	10 kNs/m	30 kNs/m	Uniform	[15]
Contact stiffness k_w	$1.61 \times 10^6 \text{ kN/m}$	$4.1 \times 10^4 \text{ kN/m}$	Normal	[15]

[2]: Banverket. *Spårgeometrihandboken BVH 586.40*. Banverket, 1996

[7]: P.J. Jensen. *Sporteknik*. Bannedanmark, 2 edition, 2016

[9]: X.Lei. *High Speed railway track dynamics. Models, algorithms and application*. Springer, 2015

[15]: J.M. Rocha. Probabilistic safety assessment of a short span high-speed railway bridge. *Elsevier*, 2014

Probabilistic assessment of turnout model

- EEM performed with $p=4$, $M=30$, $r=4$
- Results of EEM:

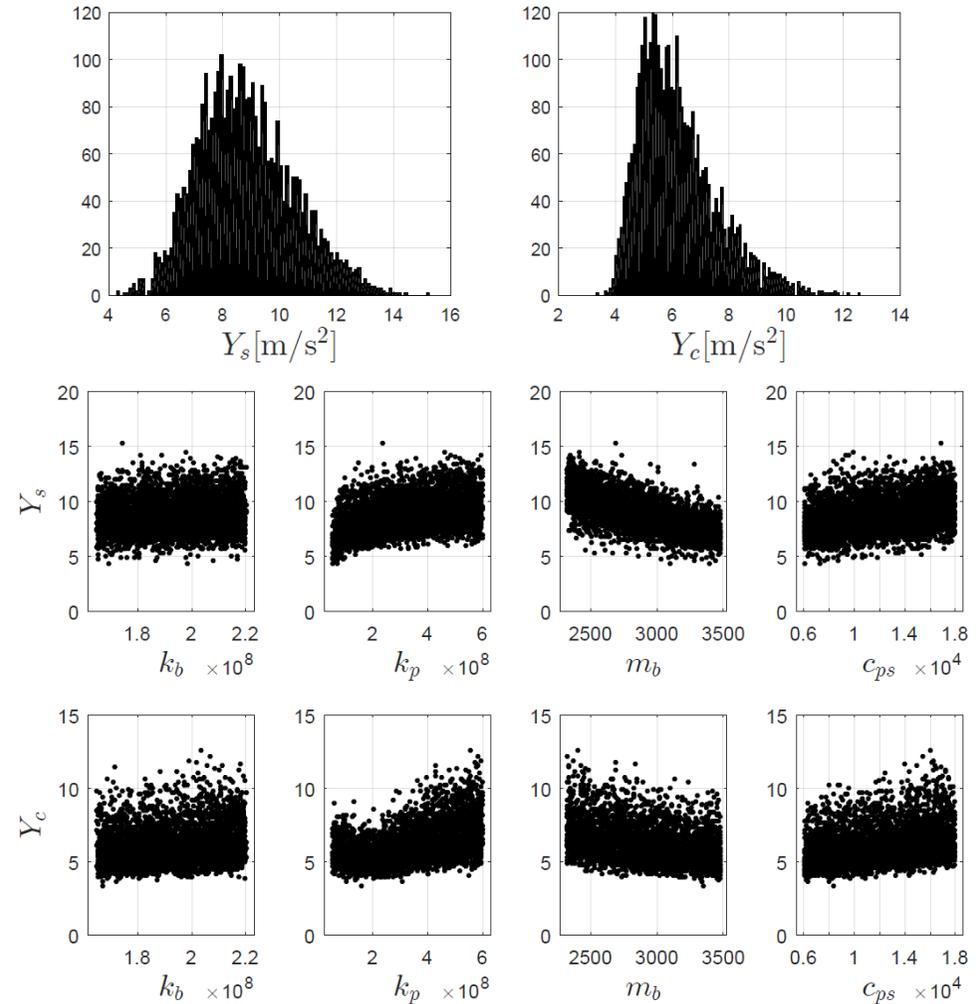
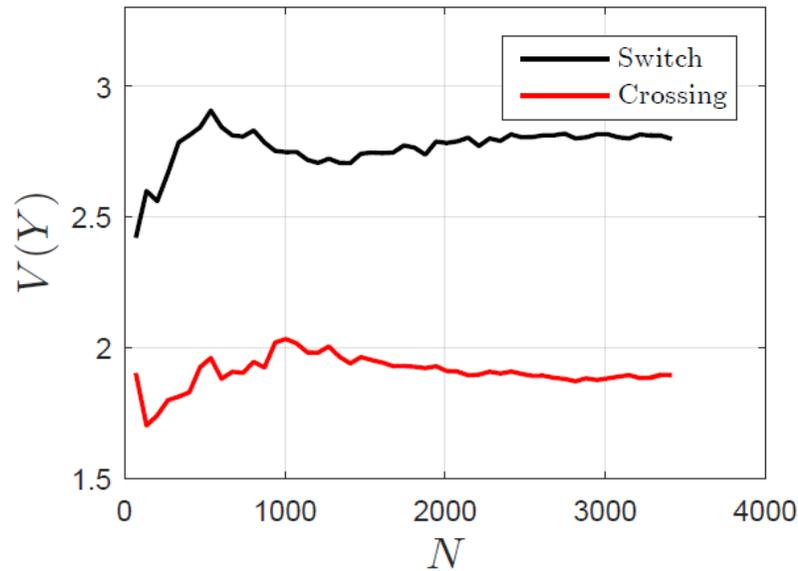
Variable	Y_s			Y_c			Rank	Score	
	μ_i^*	μ_i	σ_i^2	μ_i^*	μ_i	σ_i^2			
k_b	0.4278	0.0023	0.6129	2.0323	2.0323	1.3895	EI	0.0123	} Non-influential
c_b	0.6428	-0.6428	0.2323	0.3383	0.2476	0.4548	m	0.0610	
m_s	0.0767	0.0645	0.1345	0.1182	-0.1101	0.1112	m_s	0.0974	
k_p	3.9176	3.9176	2.7711	2.8122	2.8122	1.4169	k_w	0.2906	
c_p	0.5360	-0.5360	0.1220	0.2963	-0.1498	0.4319	c_p	0.4161	
m	0.0813	-0.0083	0.1225	0.0406	-0.0306	0.0575	c_b	0.4906	
EI	0.0102	0.0102	0.0136	0.0144	-0.0022	0.0218	c_{ss}	0.5086	
m_b	3.5622	-3.5622	0.3668	2.4156	-2.4156	1.8547	m_a	0.8427	
m_a	0.9438	-0.4790	1.0349	0.7416	-0.7416	0.1744	v	0.8905	
v	0.5202	0.3911	0.5709	1.2609	-1.0142	1.6310	k_{ps}	0.9985	
k_{ps}	0.8872	0.8872	0.7224	1.1099	1.1099	0.7448	k_{ss}	1.1111	} Most important
c_{ps}	1.7593	1.7593	0.5971	1.7779	1.7779	0.6503	k_b	1.2300	
k_{ss}	1.2354	-0.2783	1.6250	0.9868	0.6549	1.1243	c_{ps}	1.7686	
c_{ss}	0.7568	0.2488	1.1765	0.2604	-0.1044	0.2978	m_b	2.9889	
k_w	0.4856	0.1194	0.7154	0.0957	-0.0243	0.1474	k_p	3.3649	

Probabilistic assessment of turnout model

- Monte Carlo simulation with $N=3417$
Stabilize around $N=2000$

Means: $E(Y_s)=8.8 \text{ m/s}^2$ and $E(Y_c)=6.2 \text{ m/s}^2$

Variances: $V(Y_s)=2.8(\text{m/s}^2)^2$ and $V(Y_c)=1.9(\text{m/s}^2)^2$



Concluding and reflecting remarks

- Most influential variables: Railpad stiffness, bogie mass, primary suspension damping and ballast stiffness
- Least influential variables: Rail bending stiffness, rail mass, sleeper mass and contact stiffness
- Methodology capabilities: Possible to alter/remove/add input variable distributions and/or change model outputs and perform probabilistic assessment
- Improvement of methodology to increase confidence:
 - Calibrate turnout model against experimental modal analysis